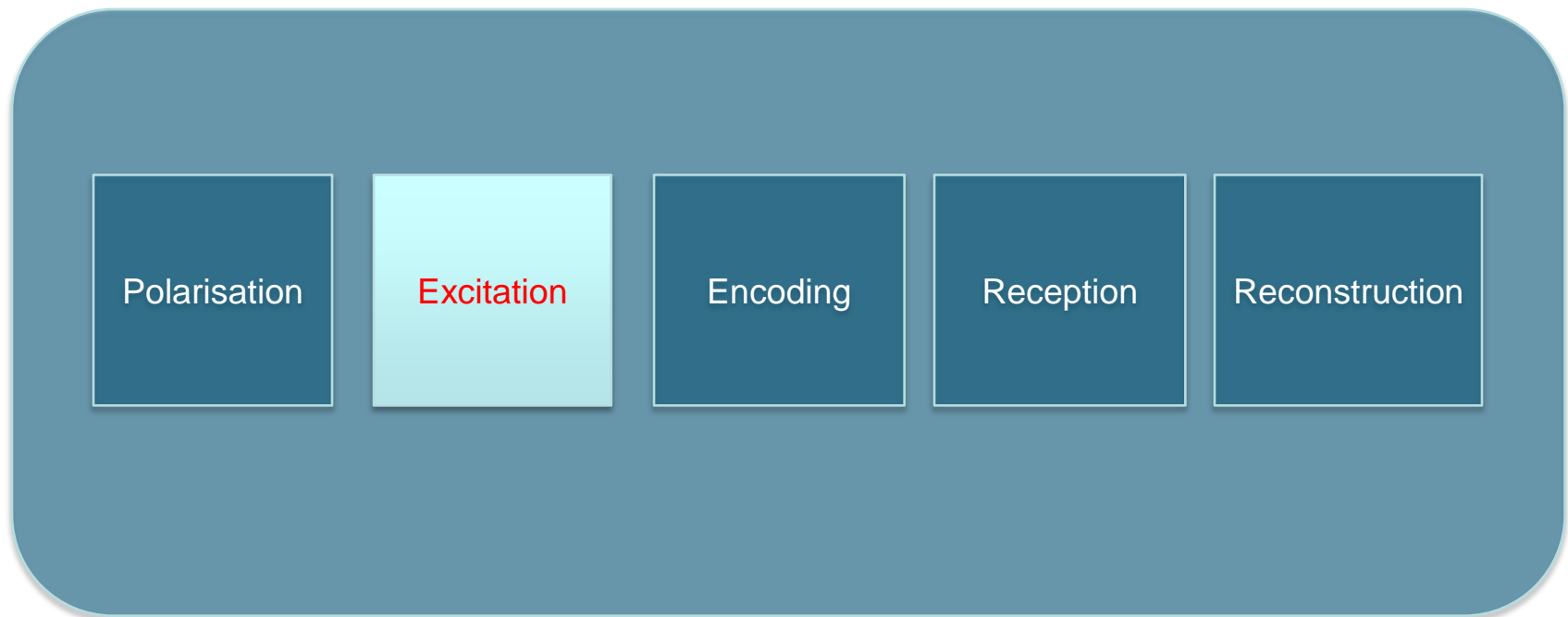


Magnetic Resonance Imaging

Excitation

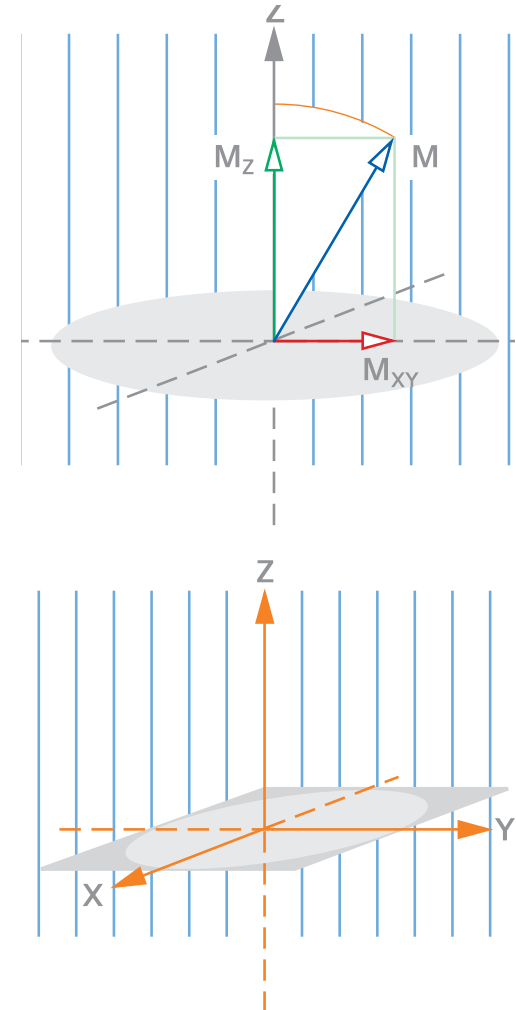
The Whole Picture



Steps of an MRI experiment

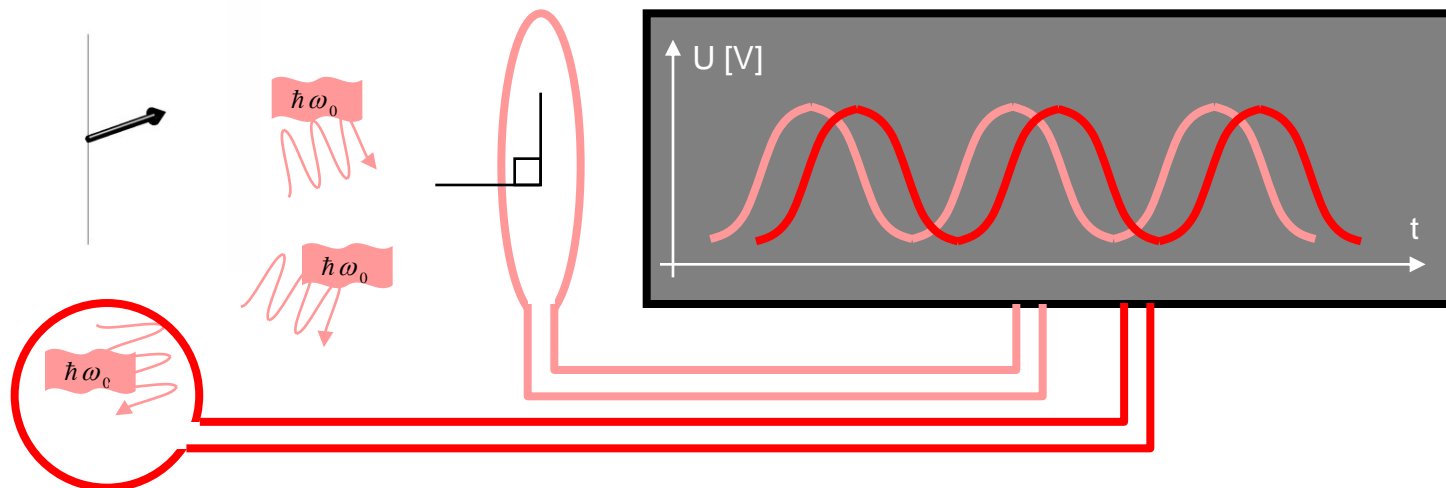
Reminder

- Longitudinal axis – z
- Sample magnetisation M
 - Transverse magnetisation ($M_x + iM_y$)
 - Longitudinal magnetisation
- External field B
 - Static B_0 (z direction)
 - RF field B_1 (x-y plane)
 - Gradient fields $dB_z/d(x,y,z)$



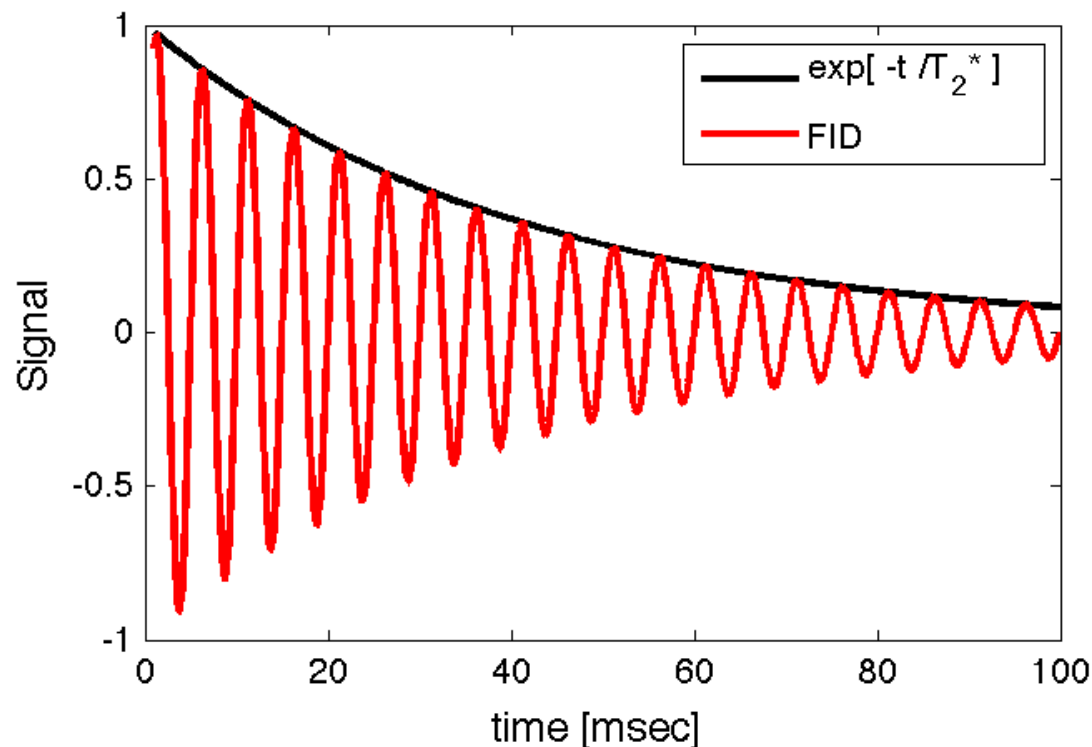
Reminder: Reception of the FID signal

- Faraday's law: detect transverse magnetization $M_{xy} = M_x + iM_y$
- Signal Equation: $S(t) \propto \int_{\text{Coil Volume}} M_{xy}(\vec{r}, t) dV$
- FID: exponential decay



Reminder: Reception of the FID signal

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Outline

- **Introduction**
- Non-selective excitation
- Off resonance effects
- Selective excitation
- Safety Considerations - SAR

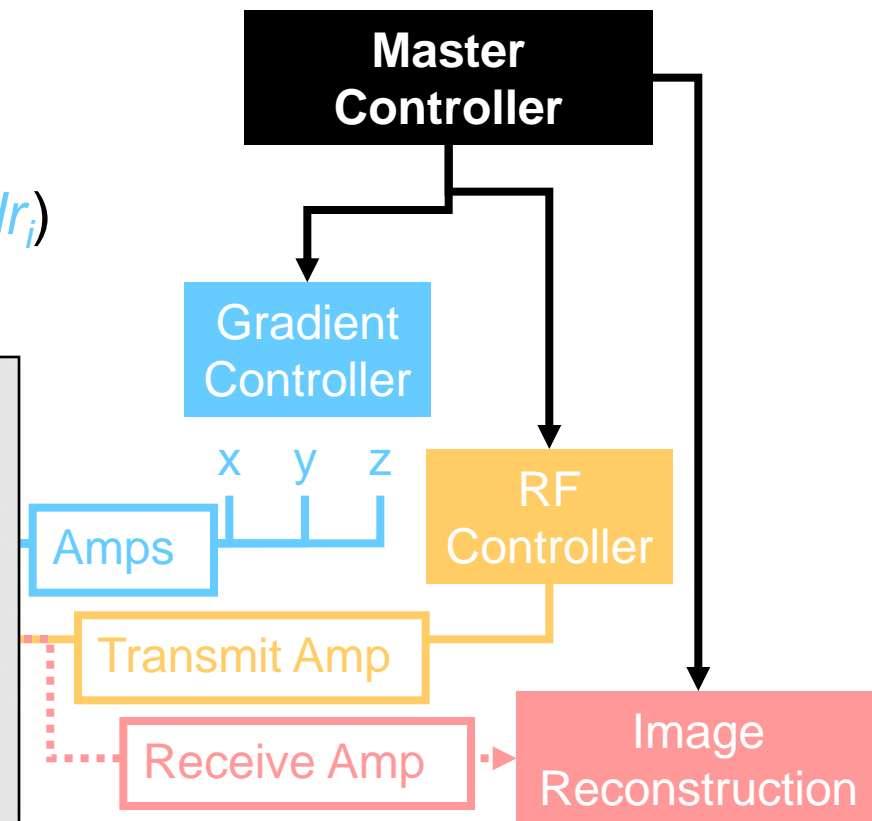
Introduction

- Excitation refers to the application of radio frequency (RF) pulses to generate transverse magnetisation
- Excitation is usually the first part of any MRI experiment
- Excitation is usually divided in
 - *Non-Selective Excitation*
 - *Selective Excitation*

MR Scanner Components (simplified)

3 Types of magnetic fields:

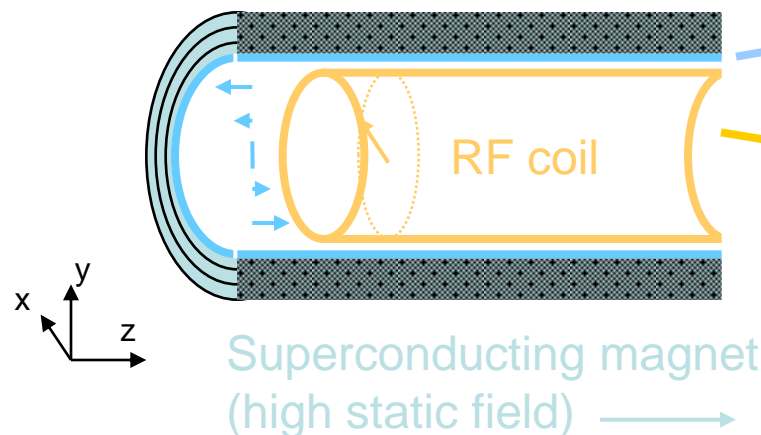
1. Static field ($B_0 \parallel z$)
2. Dynamic gradients ($G_i = dB_z/dr_i$)
3. **Radio-frequency** ($B_1 \perp z$)



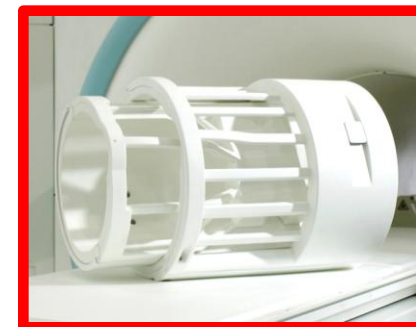
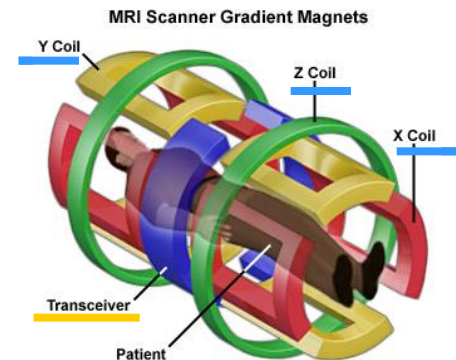
MR Scanner Components (simplified)

3 Types of magnetic fields:

1. Static field ($B_0 \parallel z$)
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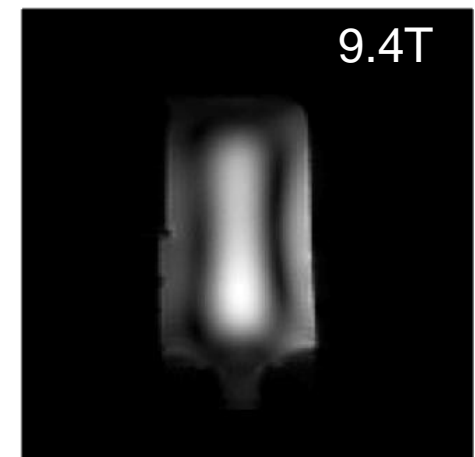
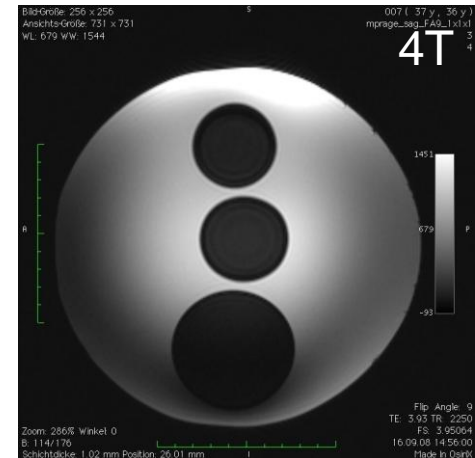


Gradient coils



RF Considerations

- Larmor frequencies of ~45...150 MHz (Field strengths 1...3T) are common
- The sensitivity of the RF coil should be as homogeneous as possible in the Volume-Of-Interest (VOI)
- Significant problems at fields > 3T
- We will assume a perfectly homogeneous RF excitation



Outline

- Introduction
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Preliminaries

- Classical picture
- Ensemble of spins (sample)
- Polarized, i.e. sample placed in the magnetic field
- Equilibrium magnetisation aligned along the z direction

The Bloch equation without relaxation

Bloch equation

$$\frac{d\mathbf{M}}{dt} = \mathbf{M} \times \gamma \mathbf{B} - \frac{M_z - M_0}{T_1} \hat{\mathbf{z}} - \frac{M_x \hat{\mathbf{x}} - M_y \hat{\mathbf{y}}}{T_2}$$

Simplification

- *No relaxation*, consider processes much shorter than the relaxation times

$$\frac{d\mathbf{M}}{dt} = \mathbf{M} \times \gamma \mathbf{B}$$

Time varying RF field

- A linearly polarised amplitude modulated radiofrequency (RF) field transmitted at frequency ω

$$B_1(t) = \hat{B}_1(t) \cdot \cos(\omega t)$$

- This decomposes into two circularly polarised RF fields
- One rotating clockwise, one rotating counter clockwise

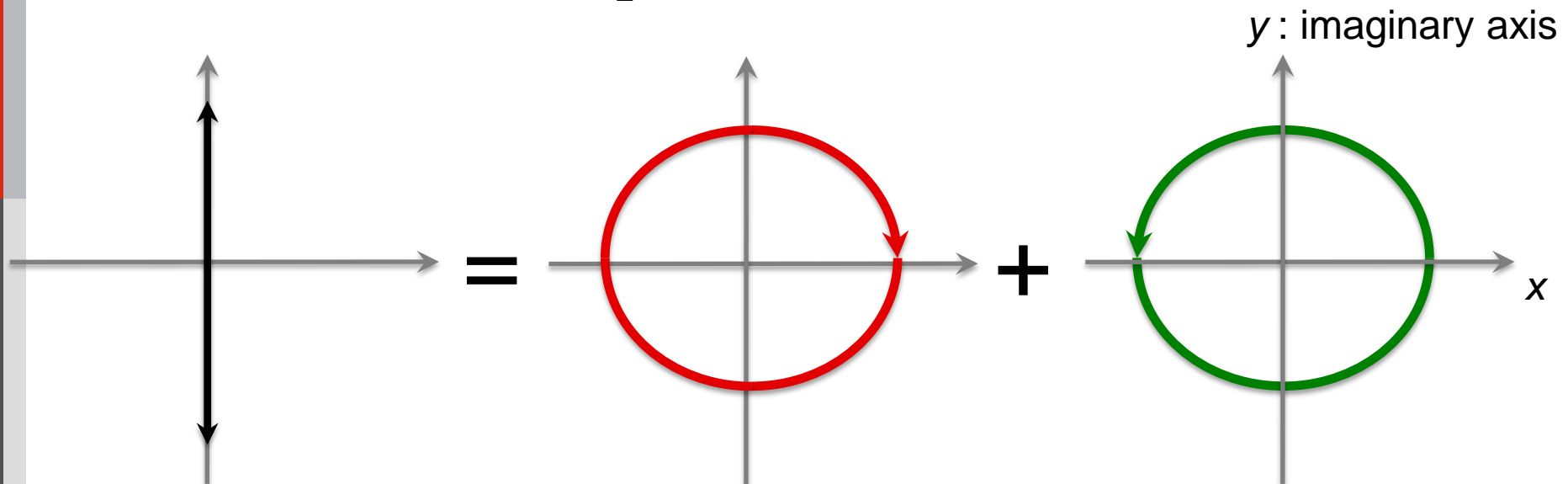
$$B_1(t) = \hat{B}_1(t) \cdot \cos(\omega t) = \frac{\hat{B}_1(t)}{2} \left(\underline{e^{-i\omega t}} + \underline{e^{+i\omega t}} \right)$$

- Only the **left** handed component affects the spins!

Time varying RF field

- Only the **left** handed component affects the spins!
- Same rotational direction as spin system → **Resonance**, if $\omega = \omega_0$!

$$B_1(t) = \hat{B}_1(t) \cdot \cos(\omega t) = \frac{\hat{B}_1(t)}{2} \left(\underline{e^{-i\omega t}} + \underline{e^{+i\omega t}} \right)$$



Time varying RF field

- RF field in complex notation $B_1(t) = \hat{B}_1 \cdot e^{-i\omega t}$
- Vector notation $B_1(t) = \hat{B}_1(t) \cdot (\cos(\omega t) \hat{x} + \sin(\omega t) \hat{y})$
- The Bloch equation without relaxation in matrix formulation for such an RF field

$$\frac{dM}{dt} = \begin{pmatrix} 0 & \gamma B_0 & \gamma \hat{B}_1(t) \sin \omega t \\ -\gamma B_0 & 0 & \gamma \hat{B}_1(t) \cos \omega t \\ -\gamma \hat{B}_1(t) \sin \omega t & \gamma \hat{B}_1(t) \cos \omega t & 0 \end{pmatrix} M$$

The rotating frame

- To simplify the above equations we move to the **rotating frame**

$$\begin{aligned} \mathbf{M} &\rightarrow \mathbf{M}_{rot} & \mathbf{B} &\rightarrow \mathbf{B}_{rot} & \mathbf{x} &\rightarrow \mathbf{x}_{rot} = \mathbf{x} \cdot \cos(\omega t) \\ & & & & \mathbf{y} &\rightarrow \mathbf{y}_{rot} = \mathbf{y} \cdot \sin(\omega t) \\ & & & & \mathbf{z} &\rightarrow \mathbf{z}_{rot} = \mathbf{z} \end{aligned}$$

- Bloch equation in the rotating frame

$$\frac{d\mathbf{M}_{rot}}{dt} = \mathbf{M}_{rot} \times \gamma \mathbf{B}_{eff}$$

The Effective Field

- A time varying amplitude modulated RF field (complex notation) transforms according as (if the coordinate system rotates with identical frequency)

$$\mathbf{B}_1(t) = \hat{\mathbf{B}}(t)e^{-i\omega t} \rightarrow \mathbf{B}_{1,rot}(t) = \hat{\mathbf{B}}(t)$$

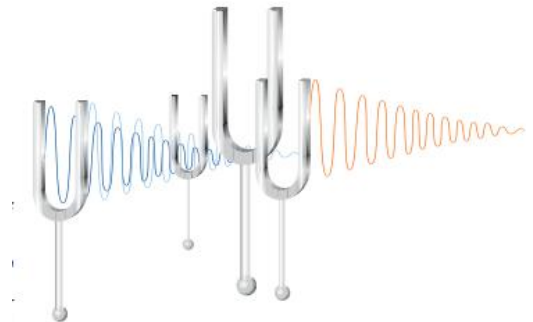
- The B field acting in the rotating frame is given as (including *off-resonances*)

$$\mathbf{B}_{eff} = \mathbf{B}_{1,rot} + \underbrace{\left(\mathbf{B}_0 - \frac{\omega_{rot}}{\gamma} \right) \hat{\mathbf{z}}}_{\text{Off resonances}}$$

On-Resonant Excitation

- In the case of *on-resonant* excitation

$$\mathbf{B}_{eff} = \mathbf{B}_{rot}$$



- We obtain

$$\frac{d\mathbf{M}_{rot}}{dt} = \begin{pmatrix} 0 & 0 & 0 \\ 0 & 0 & \gamma \hat{B}_1(t) \\ 0 & -\gamma \hat{B}_1(t) & 0 \end{pmatrix} \mathbf{M}_{rot}$$

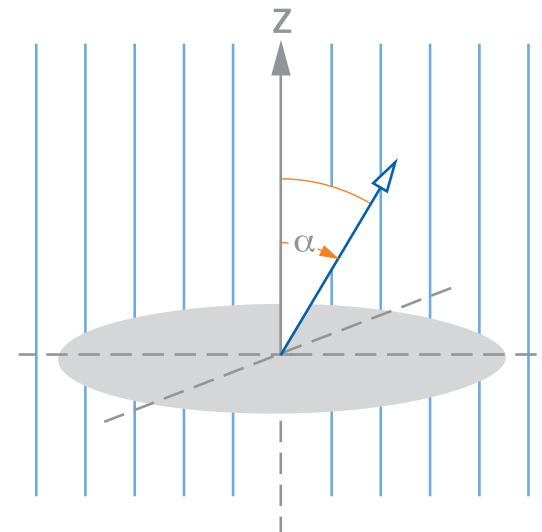
The Flip Angle

- Solution of is a rotation along the axis of the RF pulse (x in this case)

$$\mathbf{M}_{rot}(t) = \mathbf{R}_x(\alpha) \mathbf{M}_{rot}(0)$$

- The **flip angle** is given as

$$\alpha = \gamma \int_{-\tau/2}^{+\tau/2} B_1(t) dt$$



The Rectangular Pulse

- RF pulses with constant amplitude, phase and finite duration are called **Rectangular Pulses**
- In this case the flip angle is given as

$$\alpha = \gamma B_1 \tau$$

QUIZ!

**We assume a spin ensemble initially at equilibrium –
*which flip angle maximises the amount of transverse magnetisation?***

- 1) 45°
- 2) 90°
- 3) 270°

QUIZ!

You generate a rectangular RF pulse that gives rise to a flip angle of 90° .

How can you double the flip angle?

- 1) Double the duration
- 2) Double the amplitude
- 3) Double amplitude and duration simultaneously
- 4) None of the above

Outline

- Introduction
- Non-selective excitation
- Off resonance effects
- Selective excitation
- Safety considerations SAR

Off-Resonance

- Till now we considered the case of *on-resonant* excitation
- The carrier frequency of the RF field was tuned to the Larmor frequency
- System imperfections (static field inhomogeneities) and sample properties (chemical shift, susceptibility) give rise to spatially varying Larmor frequencies
- Usually off-resonances are modelled as (small) additional contributions to B_0
- Off-resonance effects on excitation

Off-Resonance

- Recall equation – off-resonances are contributions to the z component of B_{eff}

$$\mathbf{B}_{\text{eff}} = \mathbf{B}_{\text{rot}} + \left(\mathbf{B}_0 - \frac{\omega_{\text{rot}}}{\gamma} \right) \hat{\mathbf{z}}$$

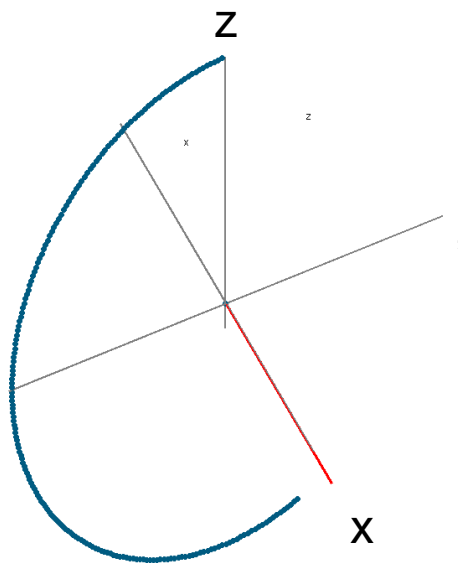
$$\gamma \mathbf{B}_0 - \omega_{\text{rot}} \equiv \Delta \omega$$

- Now consider the *off-resonance* term – **no general solution**

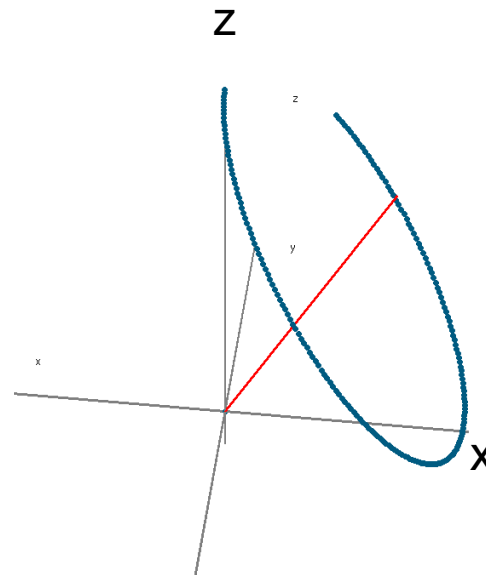
$$\frac{d\mathbf{M}_{\text{rot}}}{dt} = \begin{pmatrix} 0 & \Delta \omega & 0 \\ -\Delta \omega & 0 & \gamma \hat{B}_1(t) \\ 0 & -\gamma \hat{B}_1(t) & 0 \end{pmatrix} \mathbf{M}_{\text{rot}}$$

Off-Resonance – examples

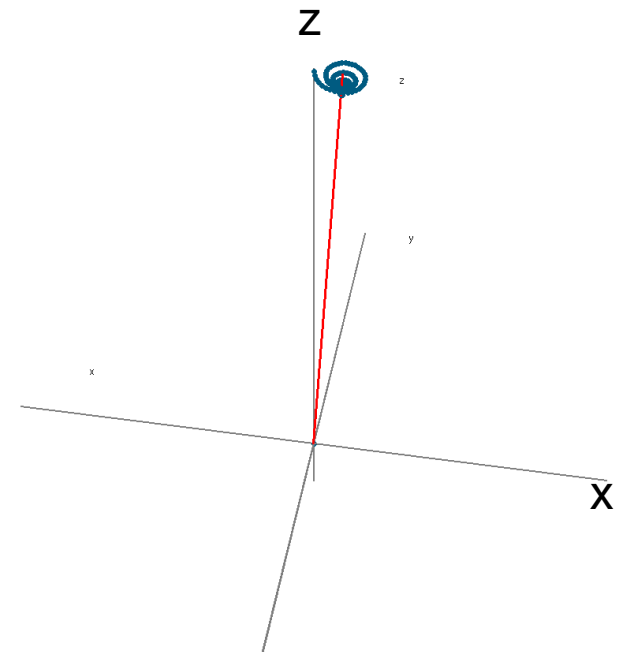
- The excitation is a precession around the **effective field**



No off-resonance

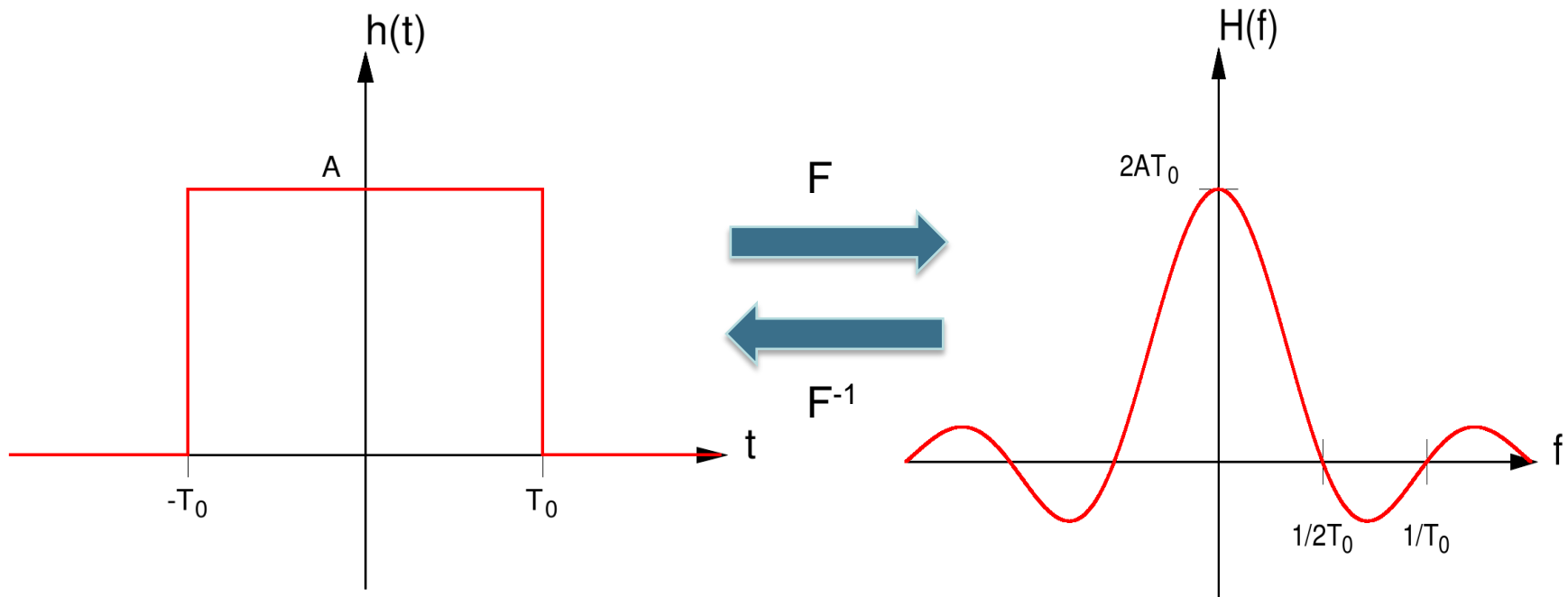


Medium off-resonance



Large off-resonance

Off-Resonance – Frequency Response of a RECT Pulse



The Effects of Off-Resonance – Summary

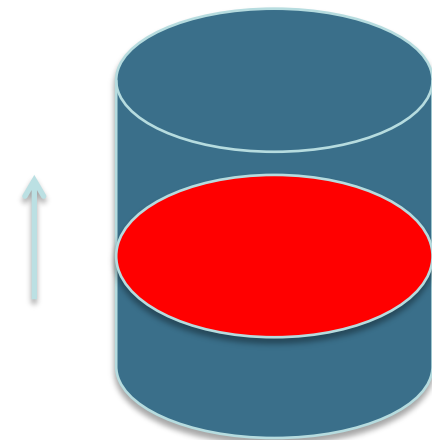
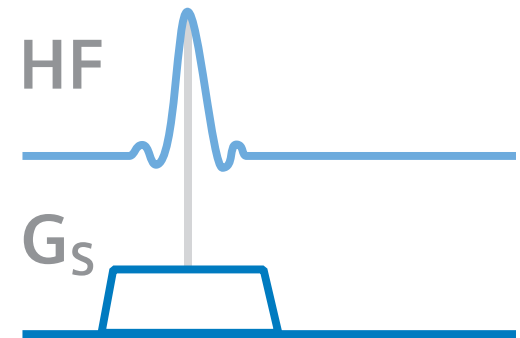
- Off-resonant spins are excited *less effective*, i.e. the flip angle is lower than without off-resonances
- Off-resonant excitation usually gives rise to a non-zero phase of the transverse magnetisation
- In the case of too large off-resonances no excitation takes place
- Controlled off-resonances (gradients) are valuable to select parts of the sample to be excited

Outline

- Introduction
- Non-selective excitation
- Off resonance effects
- **Selective Excitation**
- Safety Considerations - SAR

Silce Selection - Introduction

- Shortens the acquisition time
- Simultaneous application of gradients and RF pulses
- Slices can be created in arbitrary orientations (*double oblique*) by simultaneous application of several gradients



Silce Selection - Gradients

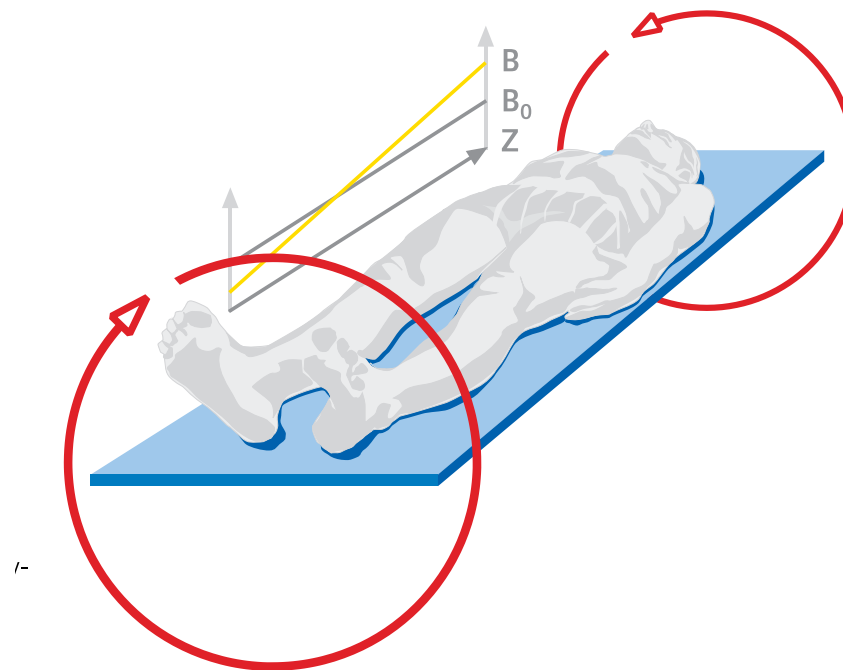
- *Gradient* in MRI usually denotes a linear field gradient of the z-component of the B field (e.g. for x direction)

$$\frac{\partial B}{\partial x} \equiv \frac{\partial B_z}{\partial x} \equiv G_x$$

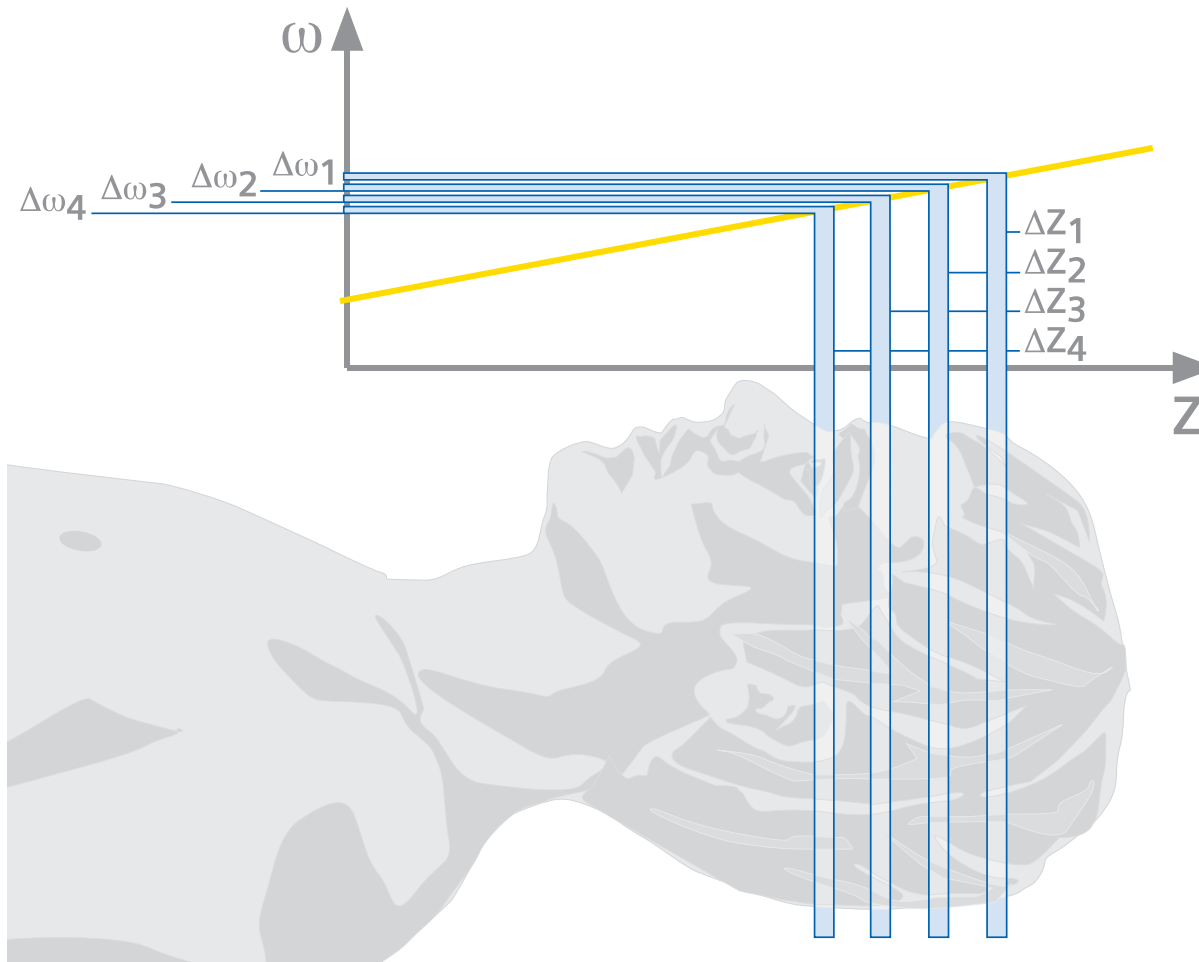
- Order of magnitude is usually '*milli Tesla per metre*' (mT/m)
- Together with the RF field (only transverse components) the time dependent magnetic field becomes

$$\mathbf{B}(t) = \mathbf{B}_1(t) + (\mathbf{B}_0 + \mathbf{G}(t) \cdot \mathbf{r}) \hat{\mathbf{z}}$$

Slice Selection - Motivation

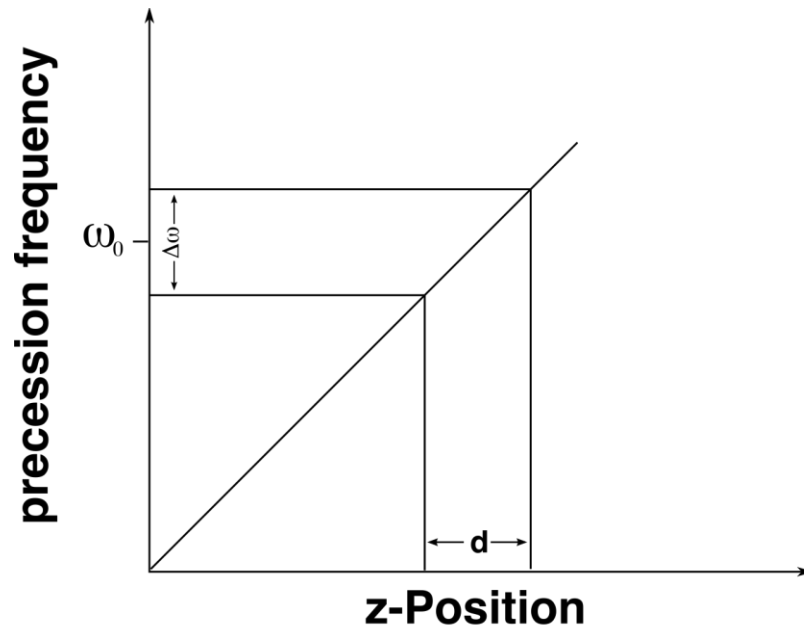


Slice Selection - Motivation

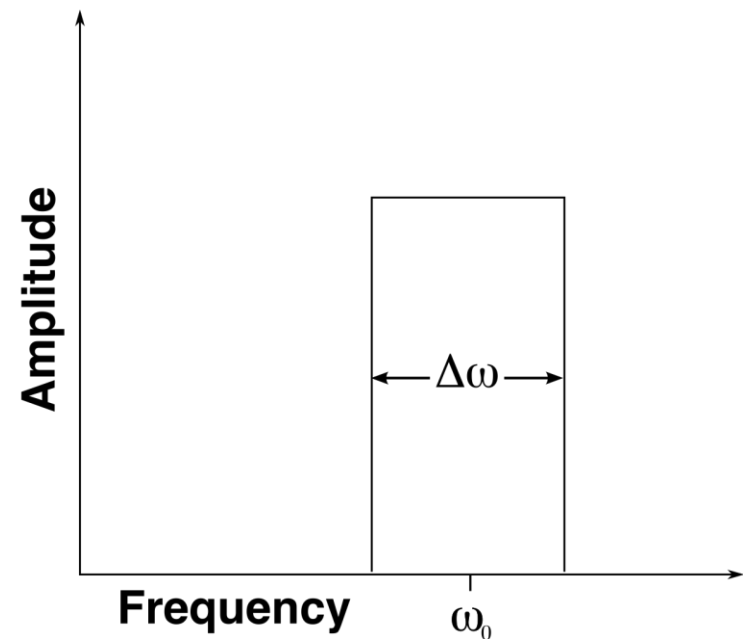


Slice Selection – Pictorial Description

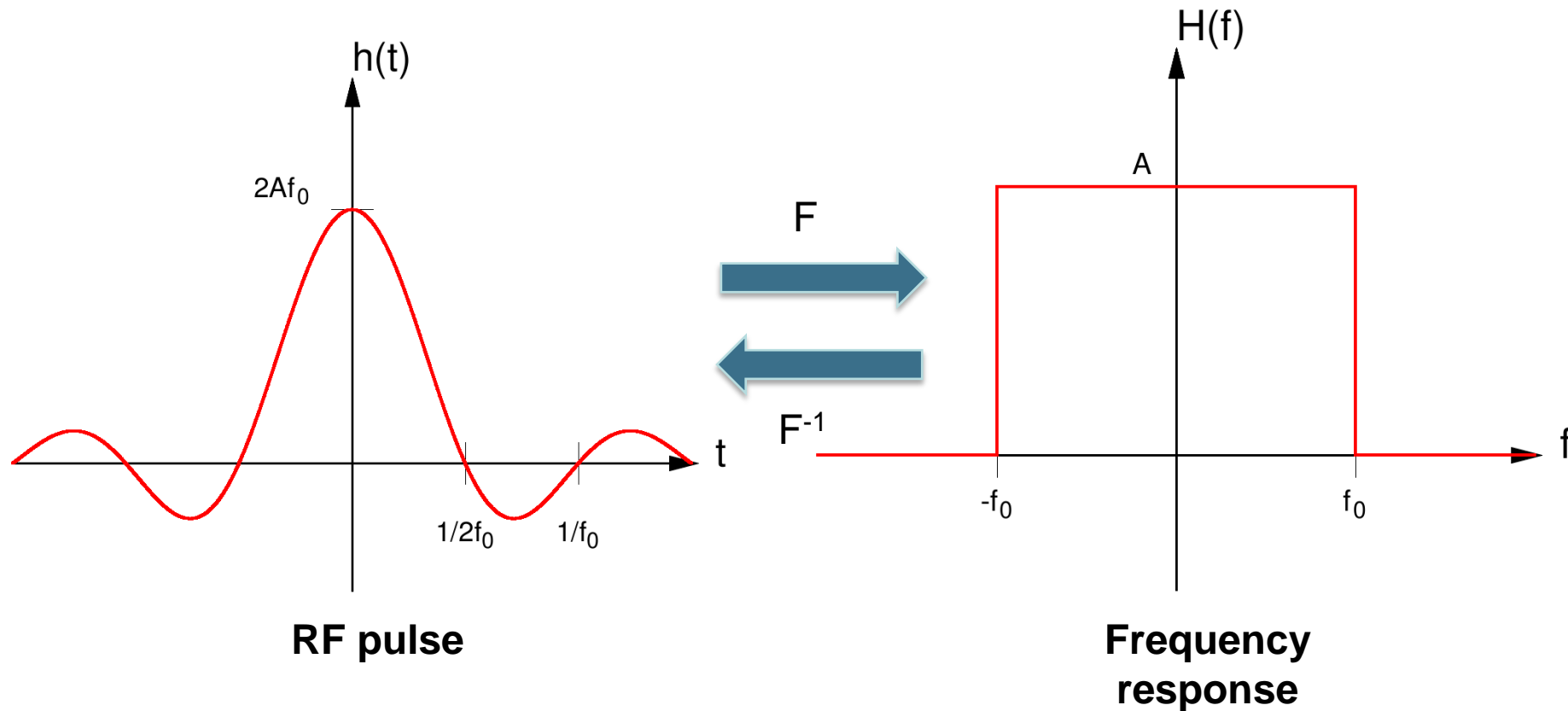
Gradient in z direction



Desired excitation



How to Excite the Desired (Rectangular) Profile?



Slice Selection – Slice Thickness

- The RF bandwidth Δf determines the *amount of frequencies* contained in a pulse
- The slice thickness is determined by the frequency band of the excitation pulse (as a function of gradient amplitude)

$$\Delta z = \frac{2\pi\Delta f}{\gamma G_z}$$

- In case of RF pulses without a rectangular freq. response (most pulses) the *Full-Width-Half-Maximum (FWHM)* is usually defined as bandwidth

Slice Selection – Bloch Equation With Gradients

- Deliberately introduce off-resonances by applying a z gradient (no other sources of off-resonance)

$$\mathbf{B}_{eff}(\mathbf{z}, t) = \mathbf{B}_1(t) + \mathbf{G}_z \mathbf{z} \hat{\mathbf{z}}$$

- Matrix formulation – again, no easy solution

$$\frac{d\mathbf{M}_{rot}(\mathbf{z})}{dt} = \begin{pmatrix} 0 & \gamma \mathbf{G}_z \mathbf{z} & 0 \\ -\gamma \mathbf{G}_z \mathbf{z} & 0 & \gamma \hat{\mathbf{B}}_1(t) \\ 0 & -\gamma \hat{\mathbf{B}}_1(t) & 0 \end{pmatrix} \mathbf{M}_{rot}(\mathbf{z})$$

Slice Selection – Small Tip Angle Approximation

- Simplify for analytical treatment
 - *Small Tip Angle* ($\sin(\alpha)=\alpha$)
 - *Constant longitudinal magnetisation* ($M_z(t) = M_0$)

$$\frac{d\mathbf{M}_{rot}(z)}{dt} = \begin{pmatrix} 0 & \gamma \mathbf{G}_z z & 0 \\ -\gamma \mathbf{G}_z z & 0 & \gamma \hat{B}_1(t) \\ 0 & 0 & 0 \end{pmatrix} \mathbf{M}_{rot}(z)$$

Longitudinal and transverse magnetisation are decoupled!

Slice Selection – Small Tip Angle Approximation

- Rewrite in complex notation – first order nonlinear differential equation

$$\frac{dM}{dt} = i\gamma G_z z M + i\gamma B_1(t) M_0$$

- Solved by

$$\omega(z) = \gamma G_z z \quad \omega_1(t) = \gamma B_1(t)$$

$$M_{xy}(t, z) = iM_0 e^{-i\omega(z)t} \int_0^t e^{i\omega(z)t'} \omega_1(t') dt'$$

Slice Selection – Small Tip Angle Approximation

- After a RF pulse of duration τ

$$M_{xy}(\tau, z) = iM_0 e^{-i\omega(z)\tau/2} \int_{-\tau/2}^{+\tau/2} e^{i\omega(z)t'} \omega_1\left(t' + \frac{\tau}{2}\right) dt'$$

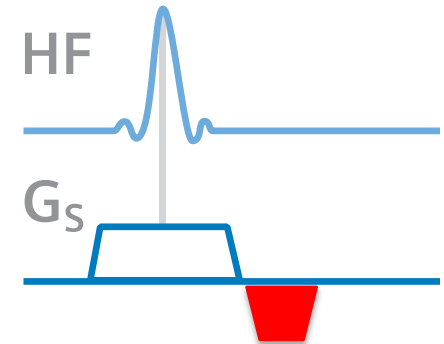
- The second term is identified as the **Fourier transform** of the applied RF pulse shape

$$M_{xy}(\tau, z) = ie^{-i\omega(z)\tau/2} M_0 F\left\{\omega_1\left(t + \frac{\tau}{2}\right)\right\}$$

Slice Selection – Rephasing Gradient

- After the pulse of duration τ

$$M_{xy}(\tau, z) = \underline{ie^{-i\omega(z)\tau/2}} M_0 F\left(\omega_1\left(t' + \frac{\tau}{2}\right)\right)$$



- Dephasing term** leads to signal cancellation
- Dephasing is linear in z and is, therefore, removed by the application of a gradient with opposite amplitude and half duration

Slice Selection – *Take Home Message*

In the *Small Tip Angle Approximation* the slice profile is given by the Fourier transform of the RF pulse shape

QUIZ!

Assume a SINC pulse with a fixed frequency response in the presence of a constant gradient in z direction.

How can you move the position of the excited slice?

- 1) Change the carrier frequency of the pulse
- 2) Change the gradient amplitude
- 3) Change the RF amplitude
- 4) None of the above

QUIZ!

Same situation – *how can you change the thickness of the slice?*

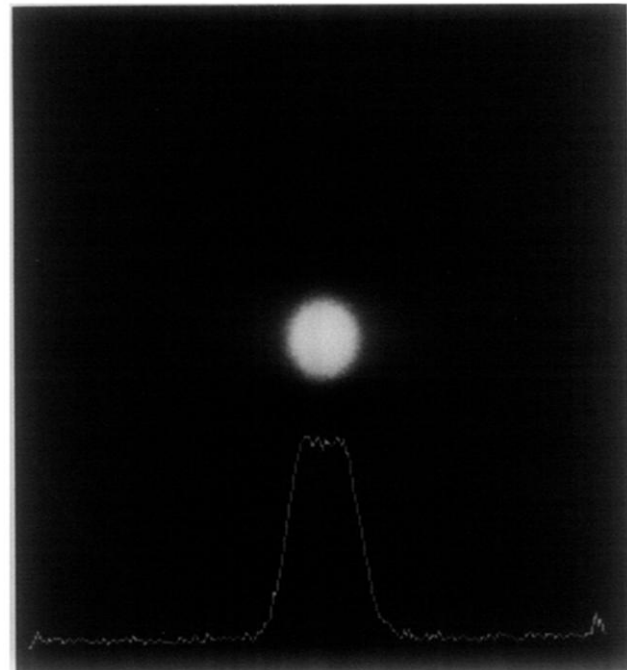
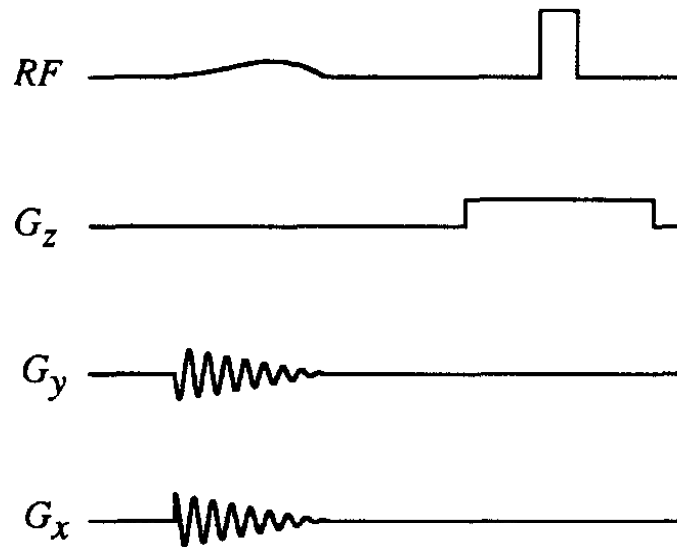
- 1) Change the carrier frequency of the pulse
- 2) Change the gradient amplitude
- 3) Change the RF amplitude
- 4) None of the above

Generalized Selective Excitation

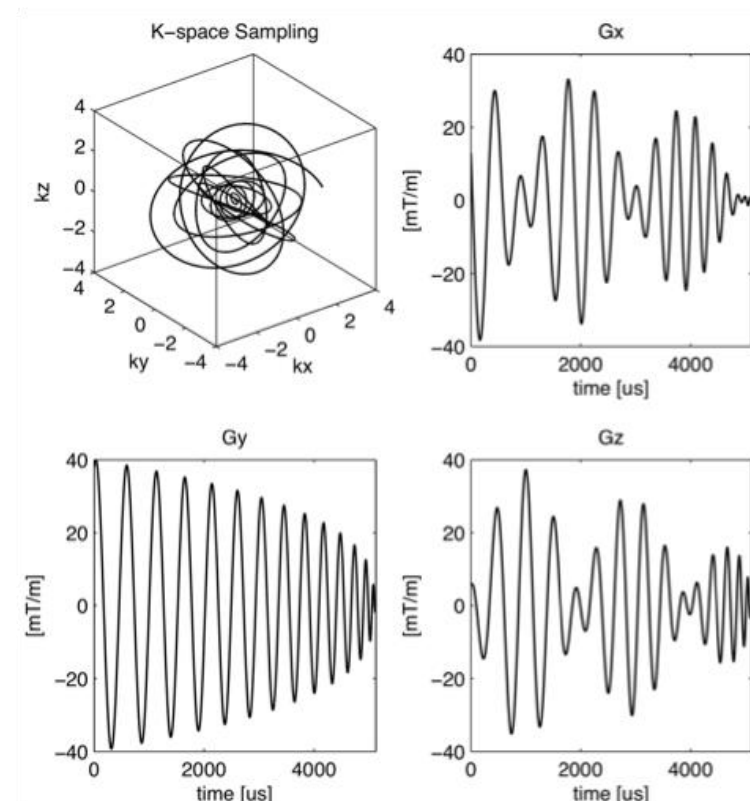
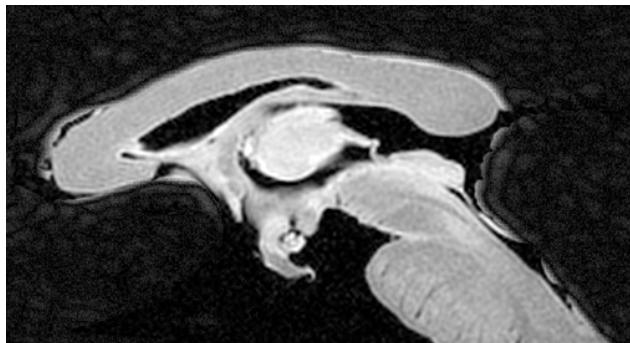
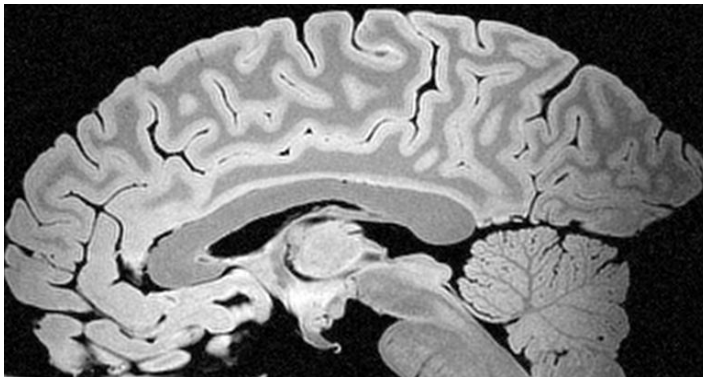
- Selective excitation is not limited to slices (1D)
- Can be extended to 2D or even higher dimensionality (3D, spatially-spectral-selective)
- Design of selective pulses is sophisticated and area of active research

Example: Pencil Beam Excitation

Pauly et al.; Journal of Magnetic Resonance 81,43-56 (1989)



Example: 3D Selective Excitation



Vahedipour et al., FZ Juelich, 2010

Outline

- Introduction
- Non-selective excitation
- Off resonance effects
- Selective excitation
- **Safety considerations - SAR**

Safety Considerations of RF Excitations

- Specified in IEC 60601-2-33 norm
- 4 W/kg averaged over the whole body for any 15-minute period
- 3 W/kg averaged over the head for any 10 minute period
- 8 W/kg in any gram of tissue in the extremities for any 5 minute period.
- Corresponding to a maximum tissue heating of 1°C
- Not applicable for UHF (> 4T) due to SAR localisations, to date (10/2010) no norm exists

SAR Calculations

- SAR is proportional to the square of the RF amplitude
- SAR is proportional to the square of the Larmor frequency (and, thus, the static field)

$$SAR \propto B_0^2 \hat{B}_1^2$$

- **Implications**
 - At higher field strengths it is necessary to reduce B_1
 - To maintain the specified flip angle one has to prolongue the RF pulses

Summary

- Excitation is performed by the application of RF pulses transmitted at Larmor frequency
- The flip angle is proportional to the amplitude of B_1 and pulse duration for non-selective excitation
- Selective excitation is performed to limit the volume that has to be imaged – to shorten acquisition times
- The profile of the excited slice is given by the Fourier transform of the RF pulse
- SAR limits impose a minimum time between RF pulses